

# Effects of $(\text{Mg}_{1/3}\text{Nb}_{2/3})$ substitution on the structure and microwave dielectric properties of $\text{Sr}_2\text{TiO}_4$ ceramics

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## ABSTRACT

$\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ( $0 \leq x \leq 0.4$ ) solid solutions were synthesized by standard solid-state reaction method for the first time, and their microwave dielectric properties were systematically investigated together with the microstructure. X-ray diffraction patterns revealed the formation of solid solutions in the whole composition range, while two kinds of secondary phases started to appear when  $x = 0.4$ . With increasing  $x$ , the dielectric constant ( $\epsilon_r$ ) was tuned from 42 to 26.3 and the temperature coefficient of resonant frequency ( $\tau_f$ ) could be successfully modified from 130 ppm/°C to 46.3 ppm/°C. Excellent combination of microwave dielectric properties with  $\epsilon_r = 28.5$ ,  $Q_f = 83,300$  GHz, and  $\tau_f = 53$  ppm/°C were obtained for the  $x = 0.3$  composition after sintering at 1500 °C for 3 h.

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## 1. Introduction

Owing to the rapid development of wireless communication technology, microwave dielectric ceramics have been playing a key role in global society. Nowadays, the applications of microwave dielectric ceramics are all-pervasive, and the recent progress in the fifth generation wireless systems (5G), intelligent transport systems (ITS), Internet of Things (IoT) has resulted in an increasing demand for low-loss dielectric materials. In order to promote the development of the novel information technologies, it is a hot issue to search for new candidates with suitable dielectric constant ( $\epsilon_r$ ), high quality factor ( $Q$ ) and near-zero temperature coefficient of resonant frequency ( $\tau_f$ ) [1].

In the past decades,  $\text{Sr}_2\text{TiO}_4$  with layered Ruddlesden-Popper structure has been receiving increasing attention in the research community. Lee et al. reported that the  $\text{Sr}_2\text{TiO}_4$  film exhibited stable chemical/physical properties and exceptionally low dielectric loss in the microwave frequency range [2]. For the bulk ceramics, our previous study has revealed the synthesis of  $\text{Sr}_2\text{TiO}_4$  ceramics, and outstanding microwave dielectric properties were also obtained ( $\epsilon_r = 42$ ,  $Q_f = 145,000$  GHz,  $\tau_f = 130$  ppm/°C) [3]. The good combination of  $\epsilon_r$  and  $Q_f$  value in  $\text{Sr}_2\text{TiO}_4$  ceramics is superior to the typical low loss candidates such as  $\text{Ba}[(\text{Co,Zn})_{1/3}\text{Nb}_{2/3}]\text{O}_3$  ( $\epsilon_r = 34.5$ ,  $Q_f \sim 97,000$  GHz,  $\tau_f \sim 0$  ppm/°C) [4]. However, the large

positive  $\tau_f$  value of  $\text{Sr}_2\text{TiO}_4$  ceramics is barely satisfactory for practical application and should be further adjusted towards zero.

Generally, there are two common routes to adjust the  $\tau_f$ , one is to form solid solutions and the other is to create composite ceramics. As the  $Q_f$  value is very sensitive to the phase compositions and the formation of composite ceramics is usually deteriorating, the manner of creating solid solutions is preferred in this work. For titanate compounds, the substitution of  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  for  $\text{Ti}^{4+}$  has been widely confirmed to be effective in optimizing the  $\tau_f$  values. Bian et al. have successfully tuned the  $\tau_f$  value of  $\text{Li}_2\text{TiO}_3$  ceramics to zero by forming  $\text{Li}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_3$  solid solutions ( $x = 0.24$ ) ( $\epsilon_r = 21$ ,  $Q_f = 200,000$  GHz,  $\tau_f = -1$  ppm/°C) [5]. Similar modifications have been also achieved in many other material systems, such as  $\text{Ca}[\text{Ti}_{0.35}(\text{Mg}_{1/3}\text{Nb}_{2/3})_{0.65}]\text{O}_3$  [6],  $\text{Ca}_4\text{La}_2\text{Ti}_2(\text{Mg}_{1/3}\text{Nb}_{2/3})_3\text{O}_{17}$  [7], etc. However, to our best knowledge, no previous reports concerning the substitution of  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  in  $\text{Sr}_2\text{TiO}_4$  ceramics have been reported. Motivated by this, it comes to be an important issue to understand the effects of  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  substitution on the microwave dielectric properties of  $\text{Sr}_2\text{TiO}_4$  ceramics and this may trigger a new breakthrough in the application of high performance microwave dielectric ceramics.

In this work,  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics are prepared via a standard solid-state reaction method for the first time. The microwave dielectric properties are systematically investigated together with the evolution of phase compositions and microstructures.

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## 2. Experimental procedure

$\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ( $x = 0.1, 0.2, 0.3$  and  $0.4$ ) ceramics were prepared via a solid-state reaction of  $\text{SrCO}_3$  (99.95%),  $\text{TiO}_2$  (99.99%),  $\text{MgO}$  (99.99%) and  $\text{Nb}_2\text{O}_5$  (99.99%) powders. The stoichiometric powders were ball-milled in ethanol media and then calcined at  $1250^\circ\text{C}$  in air for 3 h. After a second ball-milling, the powders were mixed with 4 wt% PVA solution and pressed into cylindrical pellets with 12 mm in diameter and 5 mm in height. The pellets were then sintered in the temperature range from  $1475^\circ\text{C}$  to  $1550^\circ\text{C}$  to obtain dense ceramics.

The relative density of the present ceramics was measured using the Archimedes method. The phase compositions of the sintered ceramics were determined using X-ray diffraction (XRD: D/max 2550/PC, Rigaku Co., Tokyo, Japan). Microstructures of the thermal etched surfaces were observed using scanning electron microscopy (SEM: S-3400, Hitachi, Tokyo, Japan). The microwave dielectric properties were evaluated using a network analyzer (E8363B, Agilent Technologies Inc., Santa Clara, CA). The evaluation of  $\tau_f$  was carried out in the temperature range of  $20^\circ\text{C}$ – $80^\circ\text{C}$ .

## 3. Results and discussion

Fig. 1(a) shows the XRD patterns of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics sintered at their optimal temperature. All the diffraction patterns in the compositions of  $x \leq 0.3$  can be successfully indexed according to  $\text{Sr}_2\text{TiO}_4$  (JCPDS #39-1471) and the relevant indices of crystallographic planes have been labeled. While, for  $x = 0.4$ , two kinds of secondary phases which could be matched as  $\text{Ti}_2\text{Nb}_{10}\text{O}_{29}$

and  $\text{Mg}_{1.05}\text{Ti}_{1.95}\text{O}_5$  co-exist with the main diffraction phase. For the present ceramics with layered perovskite structure, the structural stability is closely related with the size adaptability between perovskite and rock-salt layers, which is usually discussed in terms of the tolerance factor ( $t$ ) [8]. Therefore, it is inferred that the appearance of secondary phases should be mainly ascribed to the lower  $t$  at  $x = 0.4$ , which will be illustrated in the following discussion. Moreover, it also implies that the limit of  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  substitution in  $\text{Sr}_2\text{TiO}_4$  is less than 40% and further increase of  $x$  will lead to the appearance of Mg-/Nb-related secondary phases. Fig. 1(b) gives the enlarged XRD patterns of the present ceramics. With increasing  $x$ , the corresponding diffraction peaks shift gently towards the lower  $2\theta$  range, indicating a gradual expansion of unit cell. As shown in Fig. 1(c), with the substitution of larger  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  (0.667 Å) for  $\text{Ti}^{4+}$  (0.605 Å), both the cell parameters ascend monotonously with increasing  $x$ , and this further confirms that  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  has been successfully substituted into  $\text{Sr}_2\text{TiO}_4$  ceramics. Moreover, a continuous decline of  $c/a$  value is also noticed (see Fig. 1(d)). This indicates that the preferred orientation along  $c$  axis is gradually suppressed with increasing  $x$ .

The SEM images of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics are shown in Fig. 2. All the images demonstrate dense microstructures and an apparent evolution of grain morphology is observed. For  $x \leq 0.2$ , the grains generally exhibit long strip-like feature, and the columnar grains are gradually suppressed and then disappear with further increasing  $x$ . A similar result has also been reported in  $(\text{Sr}_{1-x}\text{Ca}_x)\text{SmAlO}_4$  solid solutions [9] and the gradual decline of  $c/a$  value discussed above should be responsible for this phenomenon.

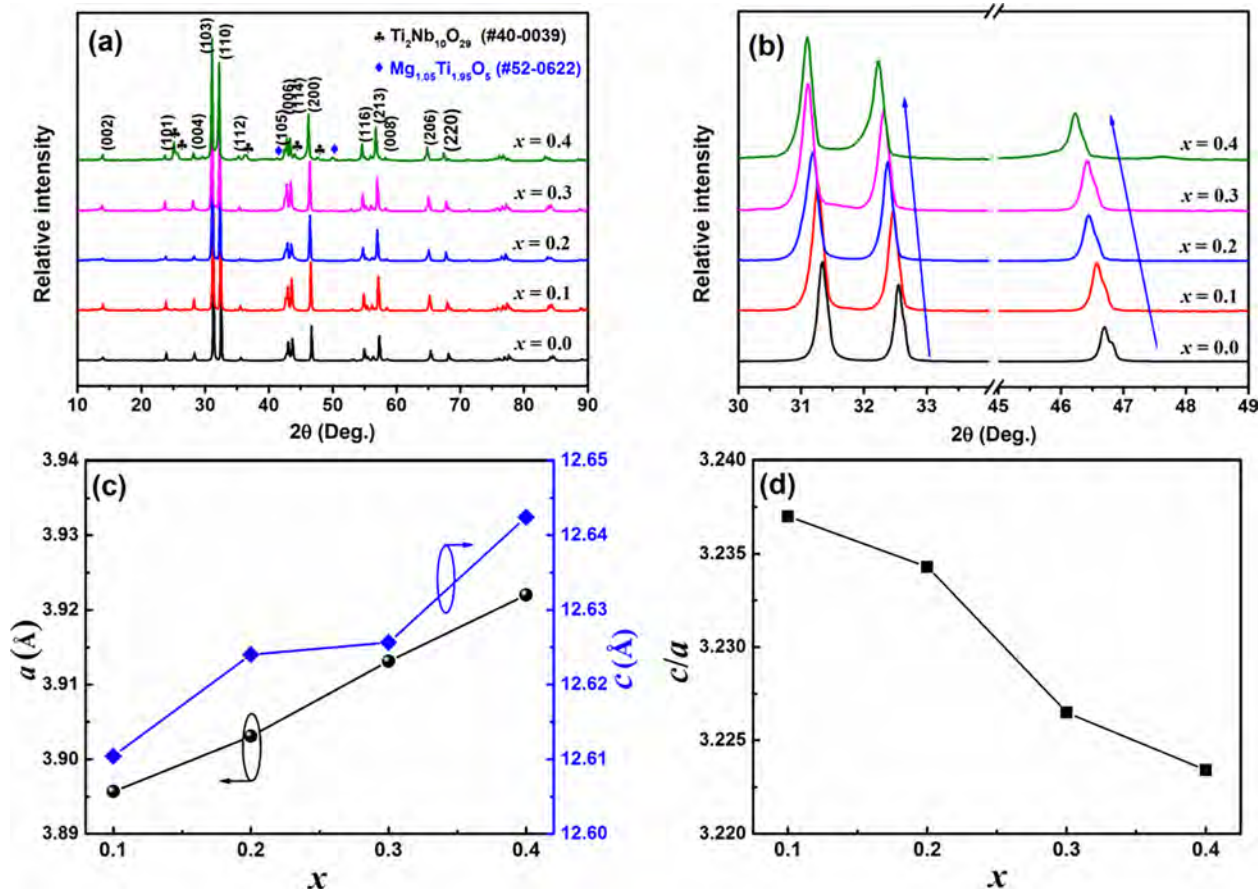
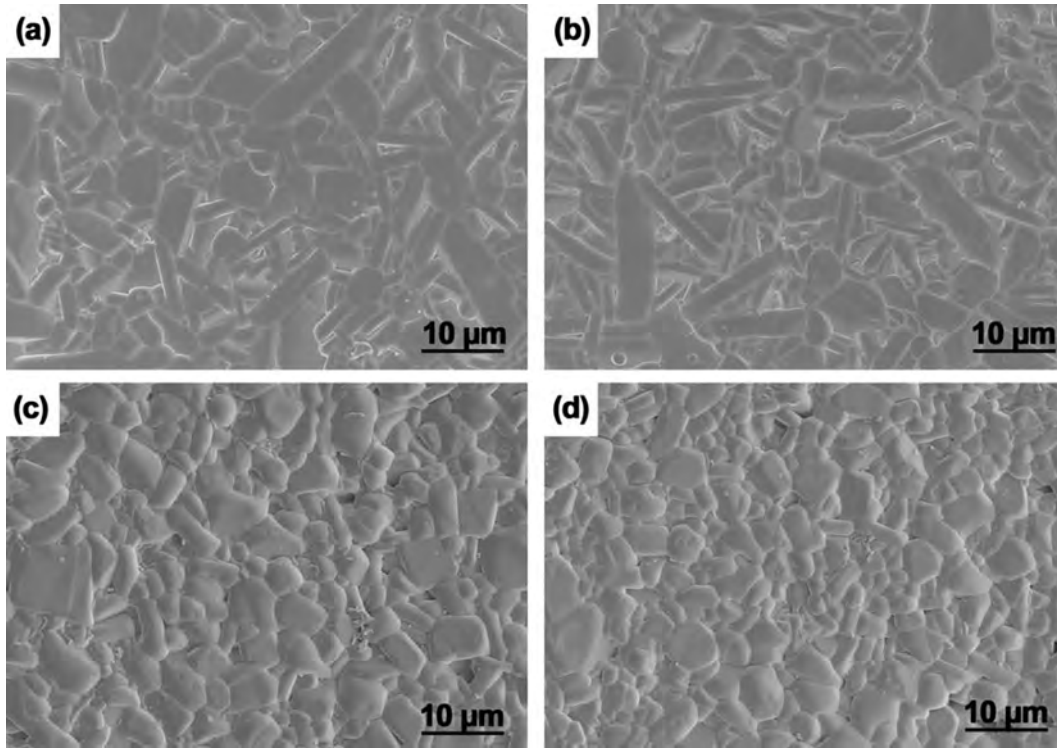


Fig. 1. (a) The XRD patterns of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics. (b) Enlargement of the diffraction patterns in the  $2\theta$  range of  $30^\circ$ – $49^\circ$ . (c, d) The lattice parameters ( $a$ ,  $c$ ) and  $c/a$  value as functions of composition  $x$ .



**Fig. 2.** The SEM images of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics: (a)  $x = 0.1$ , (b)  $x = 0.2$ , (c)  $x = 0.3$  and (d)  $x = 0.4$ .

The variation of  $\epsilon_r$  and  $\tau_f$  values of the present ceramics are plotted in Fig. 3(a).  $\epsilon_r$  decreases monotonously from 42 at  $x = 0$  to 26.3 at  $x = 0.4$ . It is notoriously known that the variation of  $\epsilon_r$  should be mainly related to the ionic polarizability per volume. According to Shannon's additive rules [10], the theoretical ionic polarizability ( $\alpha_{\text{theo}}$ ) of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics is calculated using the following equation, and the results are listed in Table 1.

$$\alpha_{\text{theo}} = 2\alpha(\text{Sr}^{2+}) + (1-x)\alpha(\text{Ti}^{4+}) + x/3 \times \alpha(\text{Mg}^{2+}) + 2x/3 \times \alpha(\text{Nb}^{5+}) + 4\alpha(\text{O}^{2-}) \quad (1)$$

where, the ionic polarizability of  $\text{Sr}^{2+}$ ,  $\text{Ti}^{4+}$ ,  $\text{Mg}^{2+}$ ,  $\text{Nb}^{5+}$  and  $\text{O}^{2-}$  are 4.24, 2.93, 1.32, 3.97 and  $2.01 \text{ \AA}^3$ , respectively [10]. With increasing  $x$ ,  $\alpha_{\text{theo}}$  increases owing to the slight larger ionic polarizability of  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  ( $3.087 \text{ \AA}^3$ ) than  $\text{Ti}^{4+}$  ( $2.93 \text{ \AA}^3$ ). The different variation tendency of  $\alpha_{\text{theo}}$  and  $\epsilon_r$  should be ascribed to the expansion of cell volume, which might lead to a lower ionic polarizability per volume.

On the other hand,  $\tau_f$  is related to the temperature coefficient of  $\epsilon_r$  ( $\tau_\epsilon$ ) and the linear thermal expansion coefficient ( $\alpha_L$ ) via the following equation [11]:

$$\tau_f = -\left(\frac{\tau_\epsilon}{2} + \alpha_L\right) \quad (2)$$

where, for most ceramics,  $\alpha_L$  is a constant value of  $\sim 10 \text{ ppm}/^\circ\text{C}$ . Therefore, the variation tendency of  $\tau_f$  is mainly determined by  $\tau_\epsilon$ , which is closely related to  $\epsilon_r$ . Consequently,  $\tau_f$  indicates a similar changing trend with  $\epsilon_r$ , and could be successfully tuned from  $130 \text{ ppm}/^\circ\text{C}$  to  $46.3 \text{ ppm}/^\circ\text{C}$ .

Fig. 3(b) shows the  $Qf$  value as functions of sintering temperature and  $x$ . For each composition, the  $Qf$  value increases with increasing sintering temperature until it reaches the maximum value at  $1500^\circ\text{C}$  or  $1525^\circ\text{C}$ , and then decreases with further increasing temperature. The optimum  $Qf$  value of each composition is plotted in Fig. 3(c). The  $Qf$  value exhibits an approximately linear decrease with increasing  $x$ , from  $145,000 \text{ GHz}$  at  $x = 0$ – $51,000 \text{ GHz}$

at  $x = 0.4$ . The decline of  $Qf$  with increasing  $x$  could be discussed from both intrinsic and extrinsic factors as the dielectric loss is sensitive to various parameters such as structural stability, phase compositions, etc. For the extrinsic part, the appearance of secondary phases at  $x = 0.4$  should be the main reason for its abnormally low  $Qf$  value. While, for the intrinsic part, the tolerance factor has been widely adopted as a reliable empirical index in predicting the structural stability and an effective parameter in correlating the intrinsic structure with the  $Qf$  value.  $t$  is calculated from the effective ionic radius of each ions using the following expression [12].

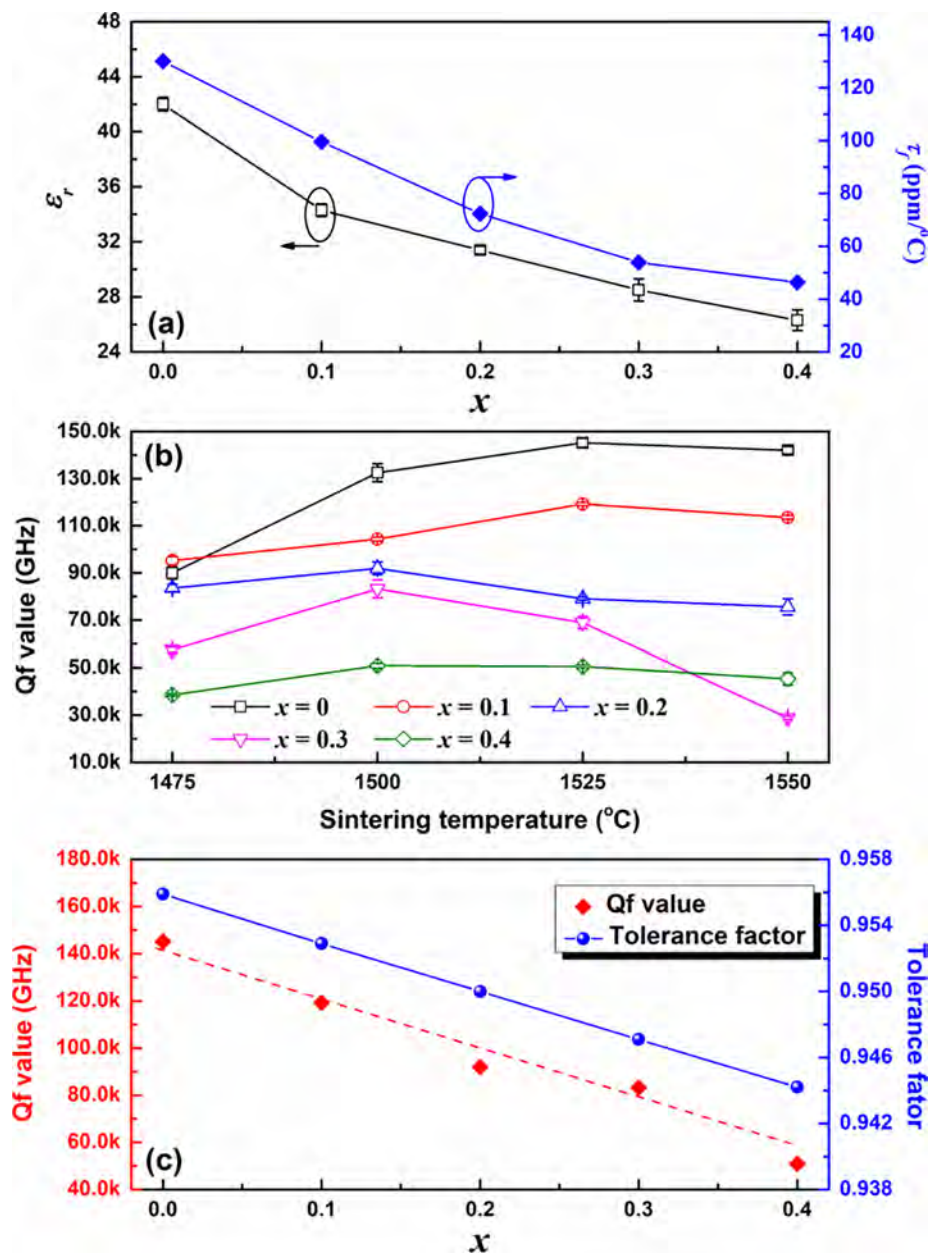
$$t = \frac{r(\text{Sr}^{2+}) + r(\text{O}^{2-})}{\sqrt{2}[(1-x) \times r(\text{Ti}^{4+}) + x/3 \times r(\text{Mg}^{2+}) + 2x/3 \times r(\text{Nb}^{5+}) + r(\text{O}^{2-})]} \quad (3)$$

The calculated  $t$  as a function of  $x$  is plotted in Fig. 3(c). The evolution of  $t$  demonstrates a similar changing trend with  $Qf$  value, indicating that the decrease of  $t$  should be another major factor affecting the  $Qf$  value. The microwave dielectric properties of each composition are summarized in Table 1 and the optimal properties are achieved at  $x = 0.3$  ( $\epsilon_r = 28.5$ ,  $Qf = 83,300 \text{ GHz}$ ,  $\tau_f = 53 \text{ ppm}/^\circ\text{C}$ ).

#### 4. Conclusions

$\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics were prepared via a standard solid state reaction method for the first time. XRD results reveal the formation of single-phased  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  solid solution in the range of  $0 \leq x \leq 0.3$ , and two kinds of secondary phases start to appear when  $x = 0.4$ . With increasing  $x$ ,  $\tau_f$  value can be successfully tuned towards zero and a good combination of microwave dielectric properties is obtained at  $x = 0.3$  ( $\epsilon_r = 28.5$ ,  $Qf = 83,300 \text{ GHz}$ ,  $\tau_f = 53 \text{ ppm}/^\circ\text{C}$ ). This indicates that the substitution of  $(\text{Mg}_{1/3}\text{Nb}_{2/3})^{4+}$  for  $\text{Ti}^{4+}$  is an effective way in adjusting the  $\tau_f$  value of  $\text{Sr}_2\text{TiO}_4$  ceramics and further modification of dielectric properties should be expected through suppressing the formation of impurities.





**Fig. 3.** (a)  $\epsilon_r$  and  $\tau_f$  values of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics as a function of  $x$ . (b)  $Q_f$  value of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics as a function of  $x$  and sintering temperature. (c) Best  $Q_f$  value of each composition as a function of  $x$ .

**Table 1**

The theoretical ionic polarizability, cell volume ( $V_m$ ), relative density and microwave dielectric properties of  $\text{Sr}_2\text{Ti}_{1-x}(\text{Mg}_{1/3}\text{Nb}_{2/3})_x\text{O}_4$  ceramics.

$x$	$\alpha_{\text{theo}} (\text{\AA}^3)$	$V_m (\text{\AA}^3)$	Sintering Temperature (°C)	Relative Density	$\epsilon_r$	$Q_f$ (GHz)	$\tau_f$ (ppm/°C)
0	19.450	190.076	1525	97.1%	42.0	145,000	130
0.1	19.465	191.379	1525	97.5%	34.3	119,000	99.5
0.2	19.480	192.316	1500	96.8%	31.4	92,000	72.3
0.3	19.495	193.329	1500	96.2%	28.5	83,300	53.0
0.4	19.510	194.468	1525	95.4%	26.3	51,000	46.3

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## Declaration of Competing Interest

We declare that we have no financial and personal relationships with other people or organizations that can inappropriately influence our work.

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